

CFD ANALYSIS OF F-16 FALCON

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ABSTRACT

Development of a fast-moving aircraft with high lift coefficient and low drag coefficient is an essential requirement for the current scenario to support to modernize the military capability of any independent Nation. In this context, the aim of our project is to examine the Viscous, Compressible and Steady-state flow over the F-16 Fighting Falcon aircraft using computer modeling techniques and to compare the modeled results with the analytical results to emphasize the modernization and warble capability. This project outlines the development of a computational model of the F-16 Fighting Falcon model in a finite computational domain, segmentation of this domain into discrete intervals, application of the boundary condition such as Mach number or velocity and then obtaining the plots and results for the coefficient of pressure, lift coefficient, drag coefficient, etc.

KEYWORDS: Aircraft, Lift Coefficient, CFD & CAD

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INTRODUCTION

The aerodynamic efficiency, which plays a major role in the design and performance of fast-moving aircraft gets support with Computational Fluid Dynamics. A CFD which changed the era in the optimization of problems in the aeronautical domain. The research carried out for the need of improved computational results in the development of more accurate results from the numerical scheme of approaches, advanced solver technology, error estimations, both numerical errors and physical model errors and in the design optimizations. CFD which plays an important role principal replacement of windtunnels in of design conditions in an accurate design, modeling of turbulent approach to complex problems [1]. To improve the military capabilities of a nation fast moving aircraft with high aerodynamic efficiencies is required. F-16 fighter falcon is the one the aircraft which has high capabilities in its performance. The F-16 is combat and multi- role fighter aircraft. The design configuration of the F-16 falcon is given in detail [2]. The main role of F-16 is it's highly manoeuvrable and has proven itself in an air-to-air combat and air to surface attack. It provides relatively low cost and high -performance weapon system for the United States [3]. The main objective here is to find the aerodynamic efficiency and to study flow analysis around the F-16 aircraft surface [4]. The flow is subjected to different Mach Conditions at subsonic, transonic and

supersonic Conditions subjecting to turbulent conditions and studying the flow effects at a different angle of attack[5]. In the simulation process, the model is subjected to both structured and unstructured grid Conditions which is studied in detailed. The effect of different types of grid conditions is studied in detail [6-8]. The flow properties of the surface, Shockwaves formed on the leading edge surface both at upper and lower surfaces with a change in Mach at different angles can be seen. The results are validated with the peer data available [9]. The results obtained for C_l , C_d , C_m and the moments on the Lockheed F-16 Falcon are accurate at the desired cases considered for different Mach (M) and Angle of attacks (α). The vortex flow interaction studies which change the pressure distribution on the surface are studied [10]. The present objective is to study the flow dynamics over F-16 fighter aircraft at different Mach Numbers (0.6 and 1.2). A CFD code has been based to investigate the performance parameters over the aircraft and the results have been obtained in terms of performance parameters. All the results are shown in forms of figure and contours and analyzed with a suitable concluding remark

METHODS

Design Specifications

Table 1

Crew:	1
Length	49 ft. 5 in (15.06 m)
Wingspan	32 ft. 8 in (9.96 m)
Height	16 ft. (4.88 m)
Wing area	300 ft ² (27.87 m ²)
Airfoil:	NACA 64A204 root and tip
Empty weight	18,900 lb (8,570 kg)
Loaded weight:	26,500 lb (12,000 kg)
Max. take-off weight	42,300 lb (19,200 kg)
Internal fuel	7,000 pounds (3,200 kg)
Power plant	1 × General Electric F110-GE-129 (for F-16C/D Block 30-40-50) or Pratt & Whitney F100-PW-220/220E afterburning turbo fan.
Dry thrust	17,155 lbf (76.3 kN)
Thrust with afterburner:	28,600 lbf (127 kN)

PERFORMANCE

Table 2

Maximum speed: At sea level:	Mach 1.2 (915 mph, 1,470 km/h)
At altitude	: Mach 2 (1,320 mph, 2,120 km/h) clean configuration
Combat radius:	340 mi (295 nmi, 550 km) on a hi-lo-hi mission with four 1,000 lb (450 kg) bombs
Ferry range:	2,280 nmi (2,620 mi, 4,220 km) with drop tanks
Service ceiling:	50,000+ ft (15,240+ m)
Rate of climb:	50,000 ft/min (254 m/s)
Wing loading:	88.3 lb/ft ² (431 kg/m ²)
Thrust/weight:	1.095 (1.24 with loaded weight & 50% internal fuel)
Maximum g-load:	+9.0 g

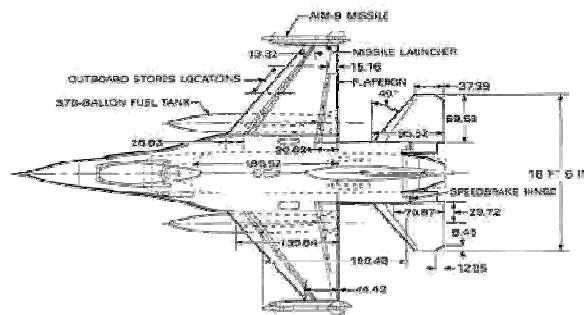


Figure 1: Top View of F-16 with Dimensions Ref (11)

METHODOLOGY

The Design and Analysis of Wing are Composed of two different approaches in computational domains: Geometry Selection and generation of geometry and importing the geometry and evaluation.

In design, the basic configuration arrangement, size, shape, and lengths are calculated. Thus, designing the CAD model of the required parts. The modeling of the F-16 Aircraft, which is used in this paper, is done using CATIA V5R20. It is a solid model over which the external flow analysis is done. Some of the sketches commands used; in this particular aircraft modeling are the line, circle, ellipse, spline, etc. And the feature commands used are loft boss, sweep boss; extrude cut, mirror, etc. While modeling this aircraft, intensive care must be taken as any improper way of modeling this may lead to overlapping of the geometry. Hence it should be seen that not two geometrical entities intersect each other. This kind of care is necessary at this stage it because later when meshing is done, it gives an enormous number of errors and would result in the poor quality mesh.

In Analysis, the generated CAD model is imported; during preprocessing the geometry (physical bounds) of the problem is defined. The volume occupied by the fluid is divided into discrete cells (the mesh). The mesh may be uniform or non-uniform. The physical modeling is defined – for example, the equations of motion + enthalpy + radiation + species conservation. Boundary conditions are defined. This involves specifying the fluid behavior and properties at the boundaries of the problem. For transient problems, the initial conditions are also defined. The simulation is started and the equations are solved iteratively as a steady-state or transient. Finally, a postprocessor is used for the analysis and visualization of the resulting solution.

The F-16 data is-

Crew:	1
Wing area:	300 ft ² (27.87 m ²)
Airfoil:	NACA 64A204 root and tip
Length	: 49 ft. 5 in (15.06 m)
Wingspan:	32 ft. 8 in (9.96 m)

ANALYSIS IN ANSYS WORKBENCH USING ANSYS FLUENT

CFD Simulation

The simulation of the continuum was done in ANSYS Fluent 16. In this initially, the meshing of the continuum was read and then checked. Once the software approves it, the scale was selected in mm as the model was created and meshed using the unit mm. Then the models, materials and boundary conditions were set.

- **Turbulence Models:** The turbulence models used for these simulations were the k- ϵ model (Realizable) and k- ω SST. The solver was based on “density-based” as the all of the simulations were compressible. Energy equations were selected in order to solve the cases as all of the simulations were compressible.
- **Materials:** The working fluid in this simulation was an ideal gas as the boundary condition “Pressure Far-field” was compatible with it. It was considered the F-16 aircraft was flying at sea level conditions and the viscosity was solved using Sutherland equations.
- **Boundary Conditions:** Pressure far-field boundary conditions were used in this simulation to model a free-stream compressible Flow at infinity, with free-stream Mach number and static conditions specified. The aircraft was given with “wall” boundary condition.
- **Solution:** The solver was a semi-implicit method for pressure-linked equations (SIMPLE) algorithm. This algorithm is an iterative procedure for solving equations for velocity and pressure, for steady-state. The Courant number is set to 2 and the under-relaxation factors for momentum and pressure are set as 0.8 and for the turbulent kinetic energy, turbulent dissipation rate and turbulent viscosity is set to 0.8. For the discretization, the pressure was kept as standard, while the other parameters Momentum, Turbulent Kinetic Energy, Turbulent dissipation Rate and Energy were retained as Second Order Upwind. Monitoring the convergence during the solution was dynamically checked by force coefficient values rather than checking for the convergence of residuals. The data were printed, reported and displayed in the plots of lift, drag, and moment coefficients, and residuals for the solution variables. On the Force Monitors, the Force vectors Lift and Drag had to define with relative to the free stream direction.

ANSYS ADAPTATION



SETUP	
GENERAL 	
Scale Domain extents	
Xmin (mm)	= -15 Xmax (mm) = 60
Ymin (mm)	15 Ymax (mm) = 15
Zmin (mm)	= -20 Zmax (mm) = 20
Check  Ok	
REPORT QUALITY	
Minimum Orthogonal Quality	= 7.77495e – 03
Maximum Ortho Skew	= 9.66586e – 01
Maximum Aspect Ratio	4.22296e+01
SOLVER	
Type	= Density Based
Velocity Formulation	Absolute
Time	Steady/Dynamic
MODELS	
Energy	On
Viscous	Realizable K-e, Standard Wall Functions
MATERIALS	
Fluid	Air
Density (Kg/M ³) [variable]	1.225 @sea-level
Cp (Specific Heat) (j/Kg-K) [constant]	1006.43
Thermal Conductivity (W/m-K) [constant]	0.0242
Viscosity (Kg/m-s) [constant]	1.7894e – 05
Solid	Aluminium
Density (Kg/M ³)	2719

Table: Contd.,	
Cp (Specific Heat) (j/Kg-K)	871
Thermal Conductivity (W/m-K)	202.4

Table

CELL ZONE CONDITIONS	
Zone	Air
Type	Fluid
Operating Pressure	101325 pascal
BOUNDARY CONDITIONS	
Domain [Pressure Far field] – Mach Number	1.2
F-16 [Wall]	Stationary Wall
Inlet [Pressure Far Field / Velocity Inlet] – Mach Number	1.2
X – Component Flow Direction	386.37
Y – Component Flow Direction	103.527
Z – Component Flow Direction	0
Outlet [Pressure Far Field / Outflow] – Mach Number	1.2
REFERENCE VALUES	
Area (m ²)	1
Density (kg/m ³)	1.225
Enthalpy (j/kg)	0
Length (mm)	1000
Pressure (Pascal)	0
Temperature (k)	0
Velocity (m/s)	1
Viscosity (kg/m-s)	1.7894e-05
Ratio of Specific Heats	1.4

SOLUTION	
Formulation	Implicit
Flux Type	Roe-FDS
Spatial Discretization	
Gradient	least Squares Method
Flow	Second Order Upwind
Turbulent Kinetic Energy	Second Order Upwind
Turbulent Dissipation Rate	Second Order Upwind
Convergence Acceleration for Stretched Mesh	
SOLUTION CONTROLS	
Courant Number	2
Under Relaxation Factors	
Turbulent Kinetic Energy	0.8
Turbulent Dissipation Rate	0.8
Turbulent Viscosity	1
Solid	1
Solution Limits	
Minimum Absolute Pressure (Pascal)	1
Maximum Absolute Pressure (Pascal)	5e+10
Minimum Static Temperature (K)	1
Maximum Static Temperature (K)	5000
Minimum Turbulent Kinetic Energy (M ² /S ²)	1e-14
Minimum Turbulent Dissipation Rate (M ² /S ³)	1e-20

Table: Contd.,	
Maximum Turbulent Viscosity Ratio	100000
Positivity Rate Limit	0.2
MONITORS	
Residuals – Convergence Criteria	0.04
C_d , C_l , C_m	F-16
Static Pressure, Dynamic Pressure, Turbulent Kinetic Energy, Turbulent Dissipation Rate	F-16
SOLUTION INITIALIZATION	
RUN CALCULATON	
Number of Iterations	10000 (Reference)
Reporting Interval	1
Check Case	Ok – Run Calculation.

MESH

In CFD Analysis, we change the incoming airflow, we get some cases. These cases are discussed below where the 3-important factor is calculated that is pressure, drag force and lift force. Due to these forces, we take so many cases for the drag and lift force are rising but a point will come where the drag and lift for values will decrease. So, let see the cases

The expected graphical results are set of residuals, lift coefficient, and drag coefficient. The contour results are in the pressure and Mach number are evaluated.

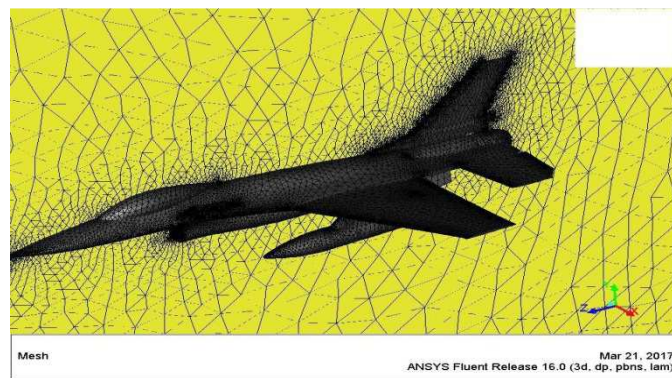


Figure 2: Mesh of the F-16

RESULTS AND DISCUSSIONS

PLOTS

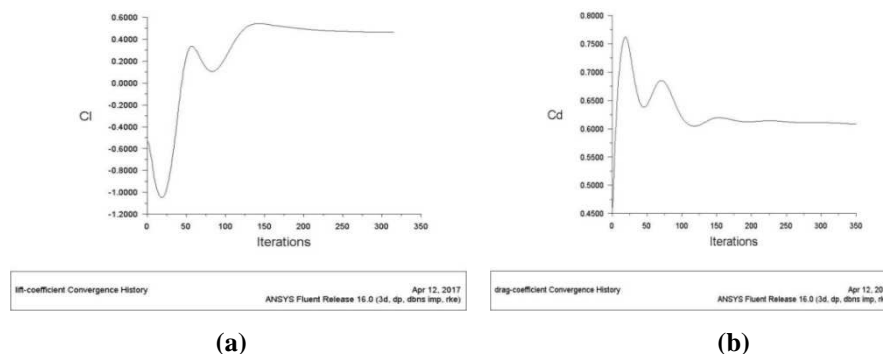


Figure 3 (a): Lift Coefficient Convergence History plot

Figure 3(b): Drag coefficient Convergence History plot

From figure 3(a), plots show that initially C_l is negative, for the supersonic fighter due to the negative stability of aircraft to take off and pitch up to steady state. From figure 3 (b) plots show that initially C_d is higher, because of the velocity decrement and there is a decrement in the drag.

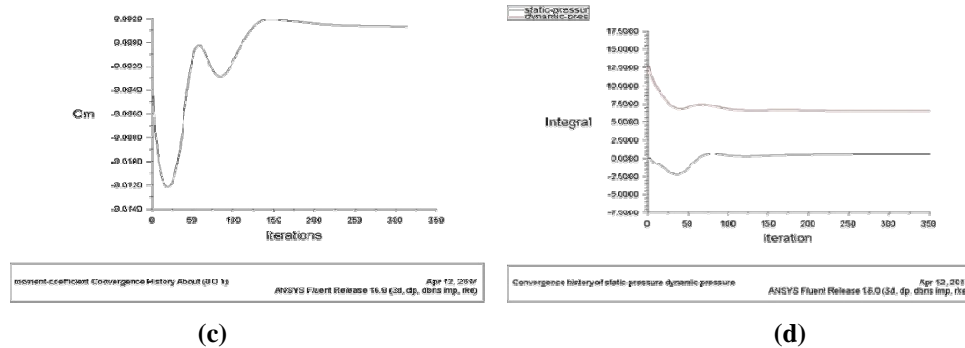


Figure 3 (c): Moment Coefficient Convergence History

Figure 3 (d): Scaled Residuals

From figure 3 (c), 3(d) one can observe that the moment Coefficient is comparatively constant

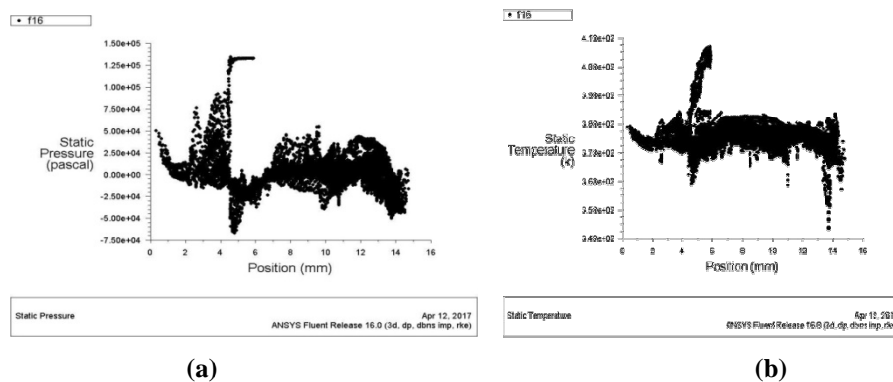


Figure 4(a): Static Pressure on F-16

Figure 4(b): Static Temperature on F-16

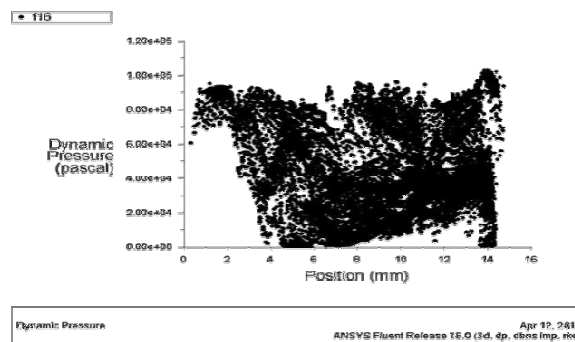
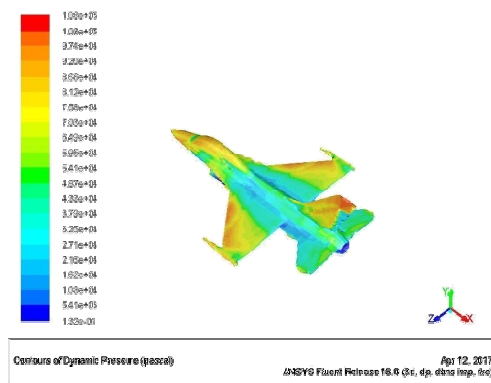
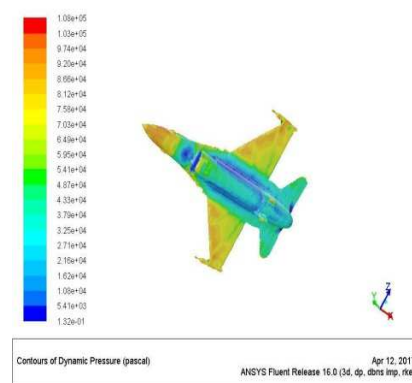


Figure 4(c): Dynamic Pressure on F-16

From figure 4(a) it can be seen that static pressure is initially decreasing and has reached to a higher level then reduced and finally maintaining the constant pressure. It's due to the surface flow interaction on the body of the F-16. From figure 4 (b) the static temperature variations can be seen. Initially, it's maintaining the constant speed then to reaching the higher level at the surface of the wing portion of aircraft because of its design, having edges and curved surfaces at the tip of the wing. From figure 4 (c) the dynamic pressure initially increasing and decreasing gradually and the distribution of dynamic pressure is varying continuously and reached to a higher level.



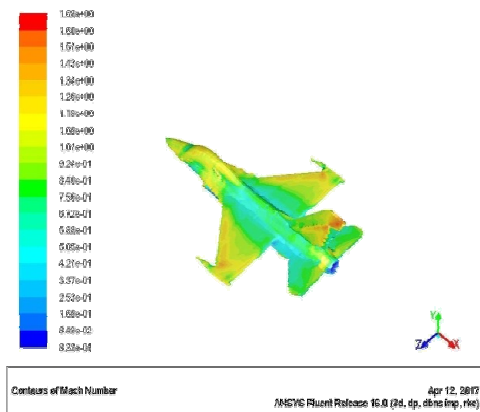
(a)

Figure 5 (a): Contours of Dynamic Pressure on F-16

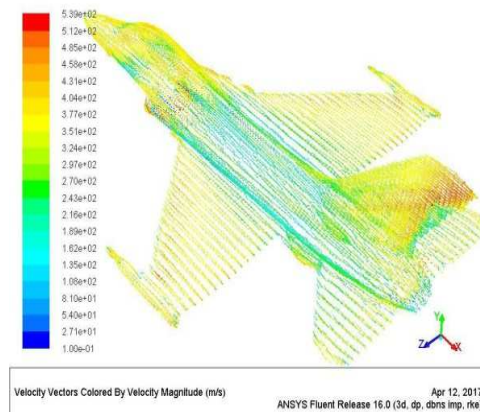
(b)

Figure 5 (b): Contours of Dynamic Pressure on F-16

From figure 5 (a), 5 (b) we can see that dynamic pressure is varying higher at a certain portion and low at the certain portion of the aircraft. This is due to the design of F-16. At the sharp edges that are a leading edge of the F-16 aircraft and at the leading edge of the wing surface at some portions of the aircraft, we can observe dynamic pressure is more. The dynamic pressure is decreasing at the tail portion of the F-16 at Mach 1 at 0 degrees AoA.



(c)

Figure 5 (c): Contours of Mach Number

(d)

Figure 5 (d): Velocity Vectors of Velocity Magnitude

From figure 5 (a), 5 (b) the variation of velocity seems to be higher at some portions and lower at some other portions on the surface of the F-16. It can be seen that the X-component velocity is higher at the curved and edge portions of the surface of F-16. As pressure is less at this portions velocity seems to be increased with increasing Mach and varying angles of attack of the aircraft by 0° , 5° , 10° , and 15° .

Velocity vs Angle of Attack

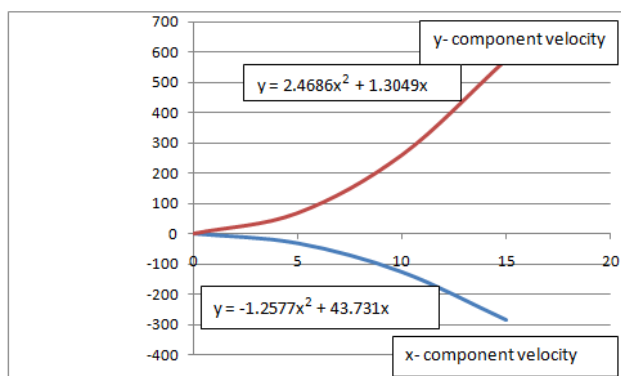


Figure 6: Flow Velocity Varying with Time and Angle of Attack

It can be seen that for a different angle of attacks that is 0, 5, 10, 15-degree angle of attack the variation in the velocity and pressure is studied on F-16 aircraft. The aerodynamic coefficients, C_l , C_d , C_m and studied and validated with the F-16 aircraft. Finally, results for velocity of X- Component and velocity of Y-Component versus different angle of attack at 0, 5, 10, 15 degree were calculated and obtained results seem too satisfy with referenced data that is X-Component velocity is decreasing with Angle of attack and Y-component of velocity seems to be increasing with increase in Angle of attack.

CONCLUSIONS

CFD analysis of F-16 aircraft was conducted and studied and compared with referred values. Here the design of the F-16 aircraft and the meshing of F-16 with accuracy play a key role. The validated mesh is chosen and then an aerodynamic analysis is done. The design of F-16 and the valued mesh chosen here for the present work gives validated results. The static pressure, dynamic pressure and aerodynamic coefficients of F-16 aircraft results are obtained. The varying of pressure, temperature, and velocity on the surface of the aircraft are clearly studied and are compared with the referred values and seems to be the nearer value of approaches. The change in velocity with a different angle of attacks was studied and is compared.

FUTURE SCOPE

The future scope of this project lies in the fact that the aerodynamic analysis of an aircraft is a vast field of research and development. So, it can be seen that the R&D can be done in the fields of aero-acoustics, fluid-structure interactions, etc. For this project, the flow is assumed to be incompressible and for a zero-degree angle of attack. So, the research can be done for compressible flow and various values of angle of attack.

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